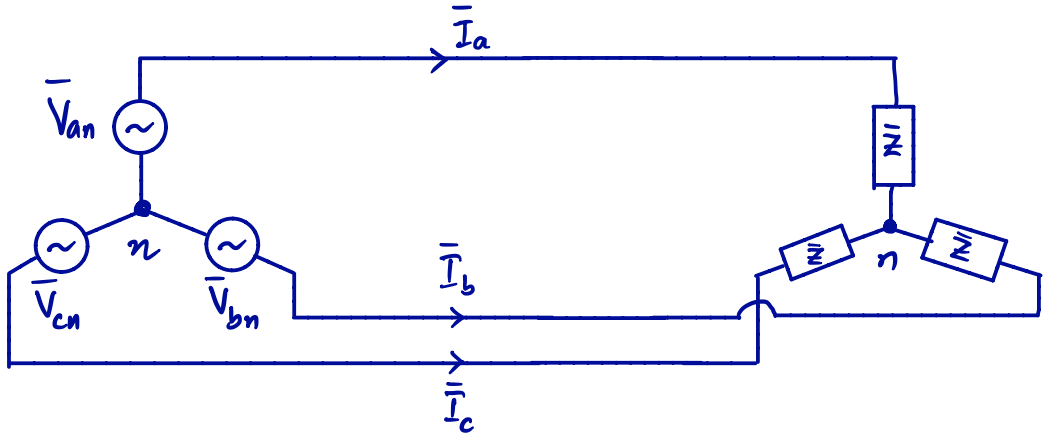
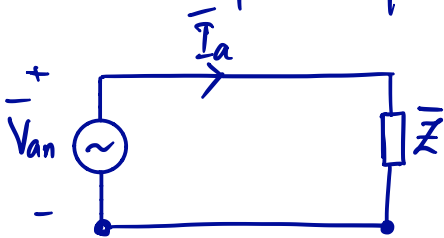


Per-phase equivalents:

• Y-source + Y-load:



Its per-phase equivalent is given by

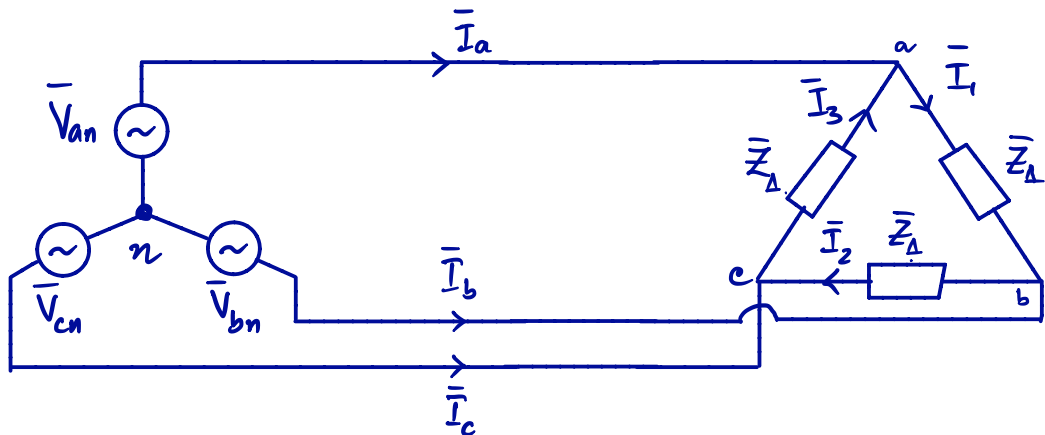


The single phase description has all information to compute all 3 ϕ quantities.

For example, $\bar{I}_a = \frac{\bar{V}_{an}}{\bar{Z}}$, and you can calculate

$$\bar{I}_b = \bar{I}_a \angle -120^\circ, \quad \bar{I}_c = \bar{I}_a \angle +120^\circ, \quad \text{etc.}$$

• Y-source + Δ load:



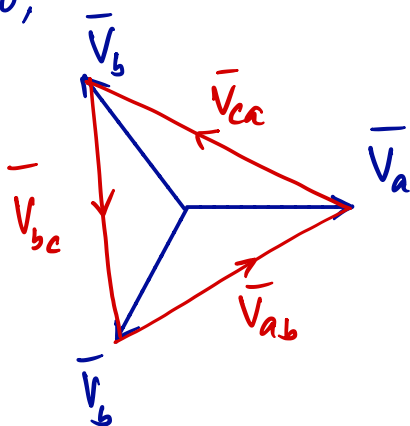
Let us transform the Δ -load to an equivalent Y-load. To simplify,

Assume that $\bar{V}_{an} = V_0 \angle 0^\circ$,

$$\Rightarrow \bar{V}_{ab} = \sqrt{3} V_0 \angle 30^\circ,$$

$$\bar{V}_{bc} = \sqrt{3} V_0 \angle -90^\circ,$$

$$\bar{V}_{ca} = \sqrt{3} V_0 \angle 150^\circ,$$

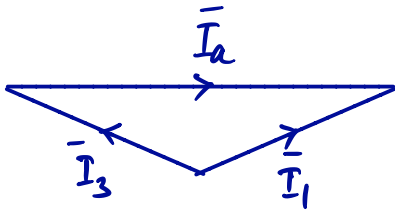


$$\bar{I}_1 = \frac{\bar{V}_{ab}}{\bar{Z}_\Delta} = \frac{\sqrt{3} V_0 \angle 30^\circ}{\bar{Z}_\Delta}$$

$$\bar{I}_2 = \frac{\bar{V}_{bc}}{\bar{Z}_\Delta} = \frac{\sqrt{3} V_0 \angle -90^\circ}{\bar{Z}_\Delta}$$

$$\bar{I}_3 = \frac{\bar{V}_{ca}}{\bar{Z}_\Delta} = \frac{\sqrt{3} V_0 \angle 150^\circ}{\bar{Z}_\Delta}$$

$$\therefore \bar{I}_a = \bar{I}_1 - \bar{I}_3 = \frac{\sqrt{3} V_0 \angle 30^\circ}{\bar{Z}_\Delta} - \frac{\sqrt{3} V_0 \angle 150^\circ}{\bar{Z}_\Delta}$$

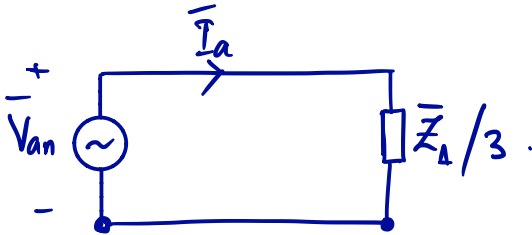


$$= \frac{1}{\bar{Z}_\Delta} \left[\sqrt{3} V_0 \angle 30^\circ - \sqrt{3} V_0 \angle 150^\circ \right]$$

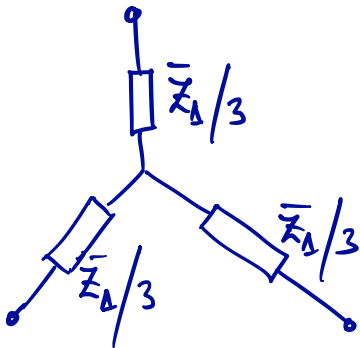
$$= \frac{1}{\bar{Z}_\Delta} \cdot \sqrt{3} V_0 \cdot \sqrt{3} \cdot \angle 0^\circ$$

$$= \frac{V_0}{\bar{Z}_\Delta / 3}$$

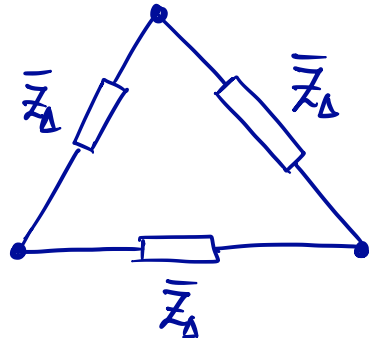
$\therefore \bar{V}_{an} = V_o \angle 0^\circ$ drives a current
 of $\bar{I}_a = \frac{V_o}{(\bar{Z}_\Delta/3)}$ through the a-phase line,
 that suggests a per-phase equivalent
 circuit given by



Then, the load is the per-phase equivalent
 of a Y-connected load with $\bar{Z}_Y = \bar{Z}_\Delta/3$,
 i.e.,



$\equiv$



... Y- Δ transformation.

Example #1

Consider a Δ -connected load with $V_L = 345 \text{ kV}$, drawing 750 MVA at a pf of 0.8 lagging.

Compute:

1. Line and phase currents.
2. Real & reactive power drawn per phase.
3. Per phase impedance.

Solution: $\therefore |\bar{S}_{3\phi}| = 750 \text{ MVA}$

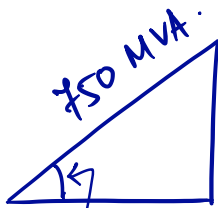
$$\Rightarrow \sqrt{3} V_L I_L = 750 \text{ MVA}$$

$$\Rightarrow I_L = \frac{750 \text{ MVA}}{\sqrt{3} V_L} = \frac{750 \text{ MVA}}{\sqrt{3} \cdot 345 \text{ kV}} = 1256 \text{ A.}$$

$$\Rightarrow I_{\phi} = \frac{I_L}{\sqrt{3}} = 725 \text{ A.}$$

2. $P_{\phi} = \frac{1}{3} \operatorname{Re}\{\bar{S}_{3\phi}\}$  Note the $\frac{1}{3}$ in front of $\operatorname{Re}\{\bar{S}_{3\phi}\}$.

$$Q_{\phi} = \frac{1}{3} \operatorname{Im}\{\bar{S}_{3\phi}\}.$$



$$\cos^{-1}(0.8) = 37^\circ.$$

$$\begin{aligned} \therefore P_\phi &= \frac{1}{3} \operatorname{Re}\{750 \angle 37^\circ\} \text{ MW} \\ &= \frac{1}{3} 750 \times 0.8 \text{ MW} \\ &= 200 \text{ MW}. \end{aligned}$$

$$\begin{aligned} Q_\phi &= \frac{1}{3} \operatorname{Im}\{750 \angle 37^\circ\} \text{ MVAR} \\ &= \frac{1}{3} 750 \times 0.6 \text{ MVAR} \\ &= 150 \text{ MVAR}. \end{aligned}$$

$$\begin{aligned} \bar{Z} &= \frac{V_\phi}{I_\phi} \angle \theta = \frac{V_L}{I_\phi} \angle \theta = \left(\frac{345 \text{ kV}}{725 \text{ A}} \right) \angle 37^\circ \Omega \\ &= 476 \angle 37^\circ \Omega. \end{aligned}$$

why?.

Example #2.

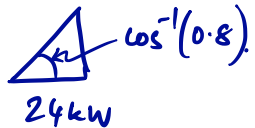
This means line-to-line voltage is 480 V.

Two 3 ϕ loads are connected in parallel to a Y-connected 480 V source:

- Y-connected load 1: 24 kW at 0.8 pf lagging
- Δ -connected load 2: 30 kVA at 0.8 pf leading.

Find the line current phasors $\bar{I}_{1,a}$ and $\bar{I}_{2,a}$ for the two loads, total complex power $\bar{S}_T$ drawn by the loads, and the total line current drawn at the source. Let $\angle \bar{V}_{an} = 0$.

Solution: $\bar{S}_{3\phi,1} = \frac{24}{0.8} \angle 37^\circ \text{ kVA.}$



$$= 30 \angle 37^\circ \text{ kVA.}$$

$$\bar{S}_{3\phi,2} = 30 \angle -37^\circ \text{ kVA.}$$

$$\therefore \bar{S}_T = \bar{S}_{3\phi,1} + \bar{S}_{3\phi,2} = 48 \text{ kW.}$$

$V_L = 480 \text{ V}$ for both loads.

$$\Rightarrow |\bar{I}_{1,a}| = \frac{|\bar{S}_{3\phi,1}|}{\sqrt{3} V_L} = \frac{30 \times 10^3}{\sqrt{3} \cdot 480} \text{ A} = 36.1 \text{ A}.$$

$\Rightarrow \angle \bar{I}_{1,a} = -37^\circ$. Why? Current lags voltage.

$$\Rightarrow |\bar{I}_{2,a}| = \frac{|\bar{S}_{3\phi,2}|}{\sqrt{3} V_L} = \frac{30 \times 10^3}{\sqrt{3} \cdot 480} \text{ A} = 36.1 \text{ A}.$$

$$\Rightarrow \angle \bar{I}_{2,a} = +37^\circ.$$

$$\therefore \bar{I}_{1,a} = 36.1 \angle -37^\circ \text{ A},$$

$$\bar{I}_{2,a} = 36.1 \angle +37^\circ \text{ A}.$$

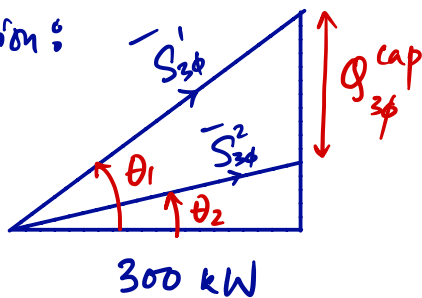
$$\text{Total line current} = \bar{I}_{1,a} + \bar{I}_{2,a}$$

$$= (36.1 \angle -37^\circ + 36.1 \angle +37^\circ) \text{ A}$$
$$= 57.7 \text{ A}.$$

Example # 3

An industrial plant consists of several 3 ϕ induction motors and draws 300 kW at 0.6 pf lagging. How much per-phase reactive power should be injected from a 3 ϕ capacitor bank in parallel to the plant to improve the net power factor to 0.9 lagging.

Solution:



$$\theta_1 = \cos^{-1}(0.6) = 53.1^\circ$$

$$\theta_2 = \cos^{-1}(0.9) = 25.8^\circ$$

Here, $\bar{S}_{3\phi}^2$ and $\bar{S}_{3\phi}^1$ are the complex powers with and without the capacitor banks.

$$\begin{aligned} \therefore Q_{3\phi}^{cap} \text{ (injected by cap banks)} &= 300 \text{ kVAR} (\tan 53.1^\circ - \tan 25.8^\circ) \\ &= 254.7 \text{ kVAR} \end{aligned}$$